

- With only one slab loaded with superimposed load,  $W_2=9.2$  and  $W_3=5.7$ .

Taking moments about centre line

$$\begin{aligned}\Sigma W e_x &= W_2 (t/3) - W_3 (t/3) \\ e_x &= (9.2 - 5.7) \times (t/3) / [9.2 + 5.7 + 177.4 + (1.4 \times 17)] \\ &= 0.5534 \text{ mm}\end{aligned}$$

From equation (5.2)

$$\begin{aligned}e_t &= 0.6 \times 0.5534 + 102.5 [(1/2400) \times (19.4)^2 - 0.015] \\ &= 0.332 + 14.536 = 14.868 \text{ mm}\end{aligned}$$

So that, since  $e_t$  is greater than  $e_x$ ,  $e_m = e_t = 0.145t$ , which is greater than  $0.05t$ , with the result that:

$$\beta = 1.1 [1 - (2 \times 0.145)] = 0.78$$

*Design vertical load resistance*

Assume  $t$  in mm and  $f_k$  in  $\text{N/mm}^2$ :

$$\begin{aligned}\text{design vertical load resistance} &= (\beta t f_k) / \gamma_m \\ &= 0.78 \times 102.5 \times f_k / 3.5 \\ &= 22.84 f_k \quad (\text{N/mm or kN/m})\end{aligned}$$

*Determination of  $f_k$*

We have

design vertical load = design vertical load resistance

$$\begin{aligned}(177.4 + 9.2 + 9.2 + 23.8) \text{ kN/m} &= 22.84 f_k \text{ kN/m} \\ f_k &= 9.61 \text{ N/mm}^2\end{aligned}$$

*Modification factors for  $f_k$*

- Horizontal cross-sectional area of wall =  $0.1025 \times 4.25 = 0.44 \text{ m}^2$ . Since  $A > 0.2 \text{ m}^2$ , no modification factor for area.
- Narrow masonry wall. Since wall is one brick thick, modification factor = 1.15.

*Required value of  $f_k$*

$$f_k = 9.61 / 1.15 = 8.35 \text{ N/mm}^2$$

*Selection of brick/mortar combination*

Use Fig. 4.1 to select a suitable brick/mortar combination. Any of the following would provide the required value of  $f_k$ .

<i>Mortar designation</i>	<i>Compressive strength of bricks (N/mm<sup>2</sup>)</i>
(iii)	35.0
(ii)	29.0
(i)	22.5

*(b) Using ENV 1996-1-1*

The dimensions, loadings and safety factors used here are the same as those given above in section (a). The reinforced concrete floor slabs are assumed to be of the same thickness as the walls (102.5 mm) and the modular ratio  $E_{\text{slab}}/E_{\text{wall}}$  taken as 2.

*Loading*

As for section (a).

*Safety factors*

For material strength,  $\gamma_m=3.0$

For loading,  $\gamma_f$  (DL)=1.35

$\gamma_f$ (LL)=1.5

*Design vertical loading (Fig. 5.16)*

Loading from above ( $W_1$ )= $1.35 \times 105 + 1.5 \times 19 = 170.25 \text{ kN/m}$

Load from left ( $W_2$ )

dead load only= $1.35 \times 4.1 = 5.535 \text{ kN/m}$

imposed load= $5.535 + 1.5 \times 2.2 = 8.835 \text{ kN/m}$

Load from right ( $W_3$ )

dead load only= $5.535 \text{ kN/m}$

imposed load= $8.835 \text{ kN/m}$

Wall self-weight= $1.35 \times 17 = 22.95 \text{ kN/m}$